

# Optimal Placement of Phasor Measurement Units using Integer Linear Programming

Naydu Vipul G.<sup>1</sup>, A. B. Parmar<sup>2</sup>

<sup>1</sup>M E Scholar, <sup>2</sup>Assistant Professor

Department of Electrical Engineering, L E College, Morbi, GTU

<sup>1</sup>[vipulnaidu25@yahoo.com](mailto:vipulnaidu25@yahoo.com), <sup>2</sup>[abparmar80@gmail.com](mailto:abparmar80@gmail.com)

**Abstract**— This paper solves the optimal placement problem of phasor measurement units (PMUs) so as to make a system completely observable. Observability assessment is done by the aid of the topological observability rules. This paper presents a generalized integer linear programming formulation for cases including redundant PMU placement, full observability. In order to improve the speed of convergence, an initial PMU placement is provided by graph-theoretic procedure. The simulation results of proposed approach are presented for several IEEE test systems.

**Keywords**— Observability analysis, optimal placement, Integer linear programming, phasor measurement unit

## I. INTRODUCTION

PHASOR Measurement Unit (PMU) was introduced in 1990s. PMU is a devices that provide synchronized measurements of real-time phasors of voltages and currents. Synchronization is achieved by same-time sampling of voltage and current waveforms using timing signals from the Global Positioning System Satellite (GPS). Synchronized phasor measurements have took the power system monitoring, control, and protection to a new level [1]. PMUs have various applications such as post-mortem analysis, adaptive protection, system protection schemes, and state estimation. One of the major issues that need to be addressed in the emerging technology of PMUs is site selection. The cost of the PMU is high so it will limit the number of installation in the system.

For PMU placement problem, the constraint condition is the observability of power system and objective function is minimizing the cost of PMU systems. In this paper algorithm for optimal placement of PMUs by using integer programming is developed.

In this paper the concept of full topological observability of the power system is adopted as the constraint condition and its principles or rules are described in section-II. PMU placement problem formulation is shown in section-III. Section-IV shows the linear algorithm. Section-V shows simulation results for standard IEEE test systems. Section-VI gives the conclusion and possible future work.

## II. OBSERVABILITY

In a power system, if a node voltage of one bus is directly measured or calculated by using other known node voltage and branch currents, then that bus is said to be observable. If all buses are observable in the system then the power system can be defined as fully observable.

There are two methods to find observability of a power system; numerical and topological. Numerical observability consists large computations and can be easily affected by cumulative error, while topological observability method is fast and practical.

In PMU placement problem, three rules can be used to analyse the topological observability if each bus within the target power system.

Rule 1: a bus with PMU installation is observable, and its adjacent buses are all observable because their voltages can be calculated by Ohm's law with the help of the PMU measurement;

Rule 2: if a bus is adjacent to an observable zero-injection bus (a bus with zero net injection of power from the connected loads and generators) to which all other adjacent buses are observable, then the bus is observable because its voltage can be calculated by KCL and Ohm's law;

Rule 3: if all buses adjacent to a zero-injection bus are observable, then the zero-injection bus is observable because its voltage can be calculated by KCL and Ohm's law.

## III. PMU PLACEMENT PROBLEM FORMULATION

A PMU placed at a bus not only gives the voltage phasor of that bus but also the current phasors of all incident branches to that bus. This makes the buses connected to the PMU bus observable. The main objective of the PMU placement problem is to make the system observable by putting the minimum number of PMUs into the system. The PMU placement function can be given as:

$$\min \sum_i^n w_i \cdot x_i \quad (1)$$

s.t.  $f(x) \geq \hat{i}$

Where,

$X$ = binary decision variable vector, defined as:

$$x_i = \begin{cases} 1 & \text{if a PMU is installed} \\ 0 & \text{otherwise} \end{cases}$$

$w_i$  is the cost of the PMU installed at bus  $i$ ;

$f(X)$ = vector function, whose value is non-zero if the corresponding bus is solvable by using the given measurement set and zero otherwise.

$\hat{i}$  = unit vector.

A PMU placed at a bus implies that the voltage of that bus and the buses connected to that bus are available or solvable. The procedure of building the constraints for the PMU placement problem is explained with the help of 7 bus system shown in figure 1.

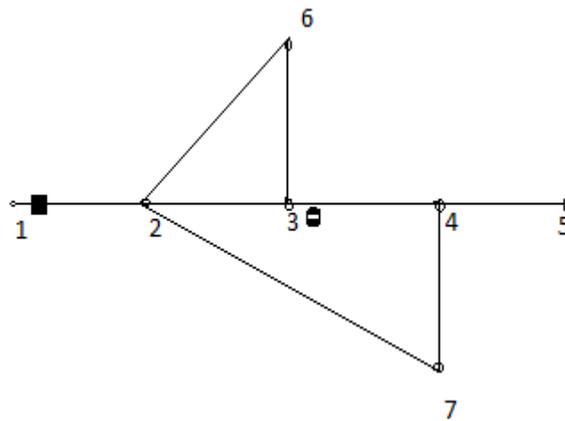


Figure 1: 7-bus system

Initially a binary connectivity matrix  $A$  is formed according to the criteria given below:

$$A_{k,m} = \begin{cases} 1 & \text{if } k = m \\ 1 & \text{if } k \text{ and } m \text{ are connected} \\ 0 & \text{if otherwise} \end{cases}$$

The connectivity matrix can also be directly obtained from the bus admittance matrix by transforming it into binary form. For the 7 bus system given in figure 1 the connectivity matrix is given as follow:

$$A = \begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 0 & 0 \\ 1 & 1 & 1 & 0 & 0 & 1 & 1 \\ 0 & 1 & 1 & 1 & 0 & 1 & 0 \\ 0 & 0 & 1 & 1 & 1 & 0 & 1 \\ 0 & 0 & 0 & 1 & 1 & 0 & 0 \\ 0 & 1 & 1 & 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 1 & 0 & 0 & 1 \end{bmatrix} \quad (2)$$

**Case 1: No conventional measurements and/or zero injections.**

The constraints for this case formed as:

$$f(X) = \begin{cases} f_1 = x_1 + x_2 & \geq 1 \\ f_2 = x_1 + x_2 + x_3 + x_6 + x_7 & \geq 1 \\ f_3 = x_2 + x_3 + x_4 + x_6 & \geq 1 \\ f_4 = x_3 + x_4 + x_5 + x_7 & \geq 1 \\ f_5 = x_4 + x_5 & \geq 1 \\ f_6 = x_2 + x_3 + x_6 & \geq 1 \\ f_7 = x_2 + x_4 + x_7 & \geq 1 \end{cases} \dots(3)$$

Here the operator “+” serves as the logical “OR” and each vector function that is f1 to f7 has to be greater than one in order to make the system observable.

The constraints mean that if bus 2 has to be made observable a PMU is needed to be placed at any of the buses among buses 1,2,3,6 and 7. It can also be considered as, if a PMU is placed at bus 2 then the buses 1,2,3,6 and 7 will be observable.

Constraints associated with bus 1 and 2 can be given as below:

$$\begin{aligned} f_1 &= x_1 + x_2 \geq 1 \\ f_2 &= x_1 + x_2 + x_3 + x_6 + x_7 \geq 1 \end{aligned}$$

The first constraint  $f_1 \geq 1$  implies that at least one PMU must be placed at either bus 1 or bus 2 (or both) to make bus 1 observable. Similarly,  $f_2 \geq 1$  indicates that at least one PMU must installed at any one of the buses 1, 2, 3, 6, or 7 to make bus 2 observable.

**Case 2: A system with injection measurements some of which may be zero injection pseudo-measurements.**

In figure 1, bus 3 is assumed to be a zero injection bus. In this case, net injected current at bus 3 is known so it is easy to find the phasor voltages at any one bus if the phasor voltage of any three out of the four buses 2, 3, 4 and 6 are known. Hence, the modified constraints associated with these buses will be given as below:

$$\begin{aligned} f_2 &= x_1 + x_2 + x_3 + x_6 + x_7 + f_3 \cdot f_4 \cdot f_6 \geq 1 \\ f_4 &= x_3 + x_4 + x_5 + x_7 + f_2 \cdot f_3 \cdot f_6 \geq 1 \\ f_6 &= x_2 + x_3 + x_6 + f_2 \cdot f_3 \cdot f_4 \geq 1 \end{aligned}$$

Note that the operator ‘.’ serves as the logical “AND”.

The expressions for  $f_i$  can be further simplified by using the following properties of the logical AND (.) and OR (+) operators: Given two sets A and B, where set A is a subset of set B, then  $A + B = B$  and  $A \cdot B = A$ . For instance, substituting the expression for  $f_3$  in the expression for  $f_2$ ,  $f_2$  can be written as:

$$\begin{aligned} &x_1 + x_2 + x_3 + x_6 + x_7 + f_3 \cdot f_4 \cdot f_6 \\ &x_1 + x_2 + x_3 + x_6 + x_7 + (x_2 + x_3 + x_4 + x_6) \cdot f_4 \cdot f_6 \\ &= x_1 + x_2 + x_3 + x_6 + x_7 + x_2 \cdot f_4 \cdot f_6 + x_3 \cdot f_4 \cdot f_6 + x_4 \cdot f_4 \cdot f_6 + x_6 \cdot f_4 \cdot f_6 \\ &= x_1 + x_2 + x_3 + x_6 + x_7 + x_4 \cdot f_4 \cdot f_6 \end{aligned}$$

Note that the expression for  $f_3$  should also include an extra product term given by  $f_2 \cdot f_4 \cdot f_6$ , however this term will be neglected.

Carrying on with the simplifications, the product  $x_2 \cdot f_4 \cdot f_6$  is eliminated because it is the subset of  $x_2$ , which already exists in the expression. Using similar reasoning,  $x_3 \cdot f_4 \cdot f_6$  and  $x_6 \cdot f_4 \cdot f_6$  are also eliminated.

Then, substitute the expression of  $f_4$  yields:

$$\begin{aligned} &x_1 + x_2 + x_3 + x_6 + x_7 + x_4 \cdot f_4 \cdot f_6 \\ &= x_1 + x_2 + x_3 + x_6 + x_7 + x_4 \cdot (x_3 + x_4 + x_5 + x_7) \cdot f_6 \\ &= x_1 + x_2 + x_3 + x_6 + x_7 + x_4 \cdot f_6 \end{aligned}$$

Since  $x_4$  is a subset of  $(x_3 + x_4 + x_5 + x_7)$ , one can write:  $x_4 \cdot (x_3 + x_4 + x_5 + x_7) \cdot f_6 = x_4 \cdot f_6$

Now, substitute for  $f_6$ :

$$\begin{aligned} & x_1 + x_2 + x_3 + x_6 + x_7 + x_4 \cdot f_6 \\ &= x_1 + x_2 + x_3 + x_6 + x_7 + x_4 \cdot (x_2 + x_3 + x_6) \\ &= x_1 + x_2 + x_3 + x_6 + x_7 \end{aligned}$$

Furthermore, having  $x_4 \cdot (x_2 + x_3 + x_6)$  as a subset of  $(x_2 + x_3 + x_6)$ , and eliminated from the expression. Finally, the expression for  $f_2$  simplifies to the following:

$$f_2 = (x_1 + x_2 + x_3 + x_6 + x_7),$$

Similarly, simplification logic to all other expressions will yield:

$$\begin{aligned} f_2 &= x_1 + x_2 + x_3 + x_6 + x_7 && \geq 1 \\ f_4 &= x_2 + x_3 + x_4 + x_5 + x_6 + x_7 && \geq 1 \\ f_6 &= x_2 + x_3 + x_6 + x_1 \cdot x_4 + x_4 \cdot x_7 && \geq 1 \end{aligned}$$

Constraints corresponding to all other buses will be same as given in equation (3). One exception is the constraint for bus 3 where the injection is known will be eliminated from the constraint set. The reason for doing this is that by removing the constraints associated with injection buses their effects are indirectly taken into account by the product terms augmented to the constraints associated with the neighbouring buses.

**Case 3: A system with injections as well as flow measurements**

The modifications needed in the formulation for this case will again be explained using the 7-bus example, in which a flow measurement (P and Q) is added for branch 1-2.

Note that having a flow measurement along a given branch, allows the calculation one of the terminal bus voltage phasors when the other one is known.

Constraints for buses 1 and 2 are merged into a joint constraint as follows:

$$\begin{cases} f_1 = x_1 + x_2 & \geq 1 \\ f_2 = x_1 + x_2 + x_3 + x_6 + x_7 & \geq 1 \end{cases} \Rightarrow f_{1\_new} = f_1 + f_2 = x_1 + x_2 + x_3 + x_6 + x_7 \geq 1$$

Which shows that if either one of the voltage phasors at bus 1 or 2 is observable, then the other one will be observable.

Applying this modification to the constraints for the 7-bus system, the set of final constraints will be obtained as follows:

$$f(X) = \begin{cases} f_{1\_new} = x_1 + x_2 + x_3 + x_6 + x_7 & \geq 1 \\ f_4 = x_2 + x_3 + x_4 + x_5 + x_6 + x_7 & \geq 1 \\ f_5 = x_4 + x_5 & \geq 1 \\ f_6 = x_2 + x_3 + x_6 + x_1 \cdot x_4 + x_4 \cdot x_7 & \geq 1 \\ f_7 = x_2 + x_4 + x_7 & \geq 1 \end{cases}$$

Note that, the constraints for buses 1 and 2 are merged into a single constraint and the constraint associated with bus 3 where there is an injection measurement, is eliminated as explained in case 2.

**IV. THE LINEAR ALGORITHM**

**Creating a Node –Incidence Matrix for Power System**

By the topological information of a power system the interconnection of the various buses can be grouped in an array called node-incidence matrix.

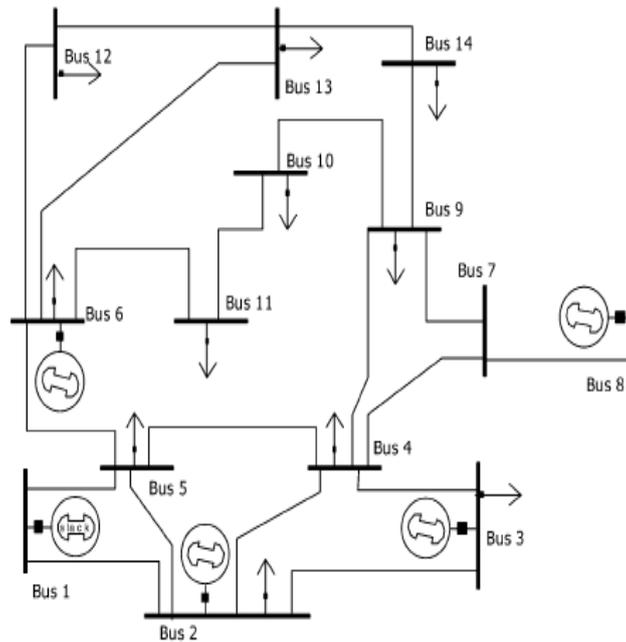


Fig. 2: IEEE-14 bus system

To produce the node incidence matrix the rule is simple: If node  $i$  is connected to node  $j$ , then  $A_{ij} = 1$ , where  $i \neq j$  and  $A_{ii} = 0$ . Normally  $A$  is a large sparse matrix. For example, for the IEEE 14-bus system,

```
A = [0 1 0 0 1 0 0 0 0 0 0 0 0 0
     1 0 1 1 1 0 0 0 0 0 0 0 0 0
     0 1 0 1 0 0 0 0 0 0 0 0 0 0
     0 1 1 0 1 0 1 0 1 0 0 0 0 0
     1 1 0 1 0 1 0 0 0 0 0 0 0 0
     0 0 0 1 0 0 0 0 0 1 1 1 1 0
     0 0 0 1 0 0 0 1 1 0 0 0 0 0
     0 0 0 0 0 0 1 0 0 0 0 0 0 0
     0 0 0 1 0 0 1 0 0 1 0 0 0 1
     0 0 0 0 0 0 0 0 1 0 1 0 0 0
     0 0 0 0 0 1 0 0 0 1 0 0 0 0
     0 0 0 0 0 1 0 0 0 0 0 0 1 0
     0 0 0 0 0 1 0 0 0 0 0 1 0 1
     0 0 0 0 0 0 0 0 1 0 0 0 1 0]
```

It is easy to find out that there are 8 nodes with degree 3 or more. Here  $K=8$  and  $n=14$ . so, the number of PMUs needed that is ,the only possible values for  $S$  between 3 and 4 using equation (1) and (2) .Now we want to find out the minimum number of PMUs, and the dominating set  $S$ . The basic idea of this algorithm is to test all possible node combinations by the observation rules, until one combination is found to be able to “observe” all the system. We call a test for a combination as a measurement. For the IEEE 14-bus system, the maximum number of measurements is number of combinations produce by selecting numbers of a group in between 3-4, who will converge, will give the required number of PMUs in the system. That is 70 for IEEE 14-bus system .We need to keep in mind that, in the implementation of the algorithm, we may not have to run all the 70 measurements to find out the  $S$ -set. The number of measurement before we get an  $S$ -set (which is usually not unique) can be any number between 1 and 70.

#### Algorithm for Finding The Minimum Number Of PMUs

##### Begin

1. Read in node-incidence matrix  $A$  with all buses (nodes) in the system says  $G$ .
2. Calculate the bounds of  $S$ .
3. Check the observability of the system by creating loop starting from the lower bound, to the upper bound:
  - a. Generate a node combination, e.g.,  $\{2, 4, 5\}$ . These nodes are mounted with PMUs, thus observed. Save them in array  $O$ .
  - b. Find out all nodes adjacent to these 3 or 4 nodes.
  - c. Save them in array  $O$ .
4. Find out all nodes that are not in  $O$ .
  - a. Pick up such a node  $j$ , use rule 4 to judge if it is observed. If yes, put  $j$  in  $O$ , and pick up another node and check.
  - b. If all “not-in- $O$ ” nodes have been checked, compare  $O$  to the whole set  $G$ .
5. If  $O=G$ , output the node combination. That is the  $S$ -set. Quit. If  $O$  is not equal to  $G$ , generate another node combination.

6. If solution does not converge then increase the numbers in the group by one toward upper bound.
7. Output how many number of combination has been tried that is the number of measurement.

**END**

## V. SIMULATION RESULTS

Simulation results without zero injections

Test system	No. of PMUs	Bus location
IEEE-14 bus	4	2, 6, 7, 9
IEEE-30 bus	10	2, 4, 6, 9, 10, 12, 15, 18, 25, 27

Simulation results with zero injections

Test system	No. of PMUs	Bus location
IEEE-14 bus	3	2, 6, 9
IEEE-30 bus	7	3, 5, 10, 12, 18, 23, 27

## VI. CONCLUSION

This paper proposes a generalized integer linear programming formulation for optimal PMU placement under different cases of redundant PMU placement, full observability and incomplete observability. This generalized formulation, considering the situations with and without zero injection measurements, shows that the problem of optimal PMU placement can be modeled linearly and can be solved by integer linear programming. The generalized formulation paves an efficient way for future research in PMU placement and related topics. From the simulation results we can see that the proposed algorithm is computationally efficient and can be used in practice.

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