To Study the Trends of Activation Energy in Metal Extractions Process

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Abstract -The project aim set study of thermal behavior, thermal degradation kinetics, and effect of composition on flow characterization of blast furnace slag is important to Understanding the flow characteristics of blast furnace (B/F) slag. It is an important parameter for efficiency/productivity of a blast furnace. In the present study flow characteristics of five different B/F slag will be investigated. This study is predominantly based on the estimation of activation energy. The activation energy was estimated using two methods: differential scanning calorimetry (DSC) and High temperature viscometer. Activation energy can be estimated from such DSC plots using Kissinger and Ozawa methods. It has observed that activation energy is largely dependent on C/S ratio of B/F Slag – The activation energy decreases with increase in C/S ratio. The flow characteristics of different B/F slag were also investigated by high temperature heating microscope, Differential scanning calorimetry (DSC). The estimated IDT (initial deformation temperature), ST (softening temperature), HT (hemispherical temperature) and FT (fusion temperature) of different B/F slag was shown in table

Index Terms – Blast Furnace, Activation Energy, DSC

I. INTRODUCTION

Most reactions involving neutral molecules cannot take place at all until they have acquired the energy needed to stretch, bend, or otherwise distort one or more bonds. This critical energy is known as the activation energy of the reaction. Higher temperatures, faster reactions: It is common knowledge that chemical reactions occur more rapidly at higher temperatures. Everyone knows that milk turns sour much more rapidly if stored at room temperature rather than in a refrigerator, butter goes rancid more quickly in the summer than in the winter, and eggs hard-boil more quickly at sea level than in the mountains. For the same reason, cold-blooded animals such as reptiles and insects tend to be noticeably more lethargic on cold days. It is not hard to understand why this should be. Thermal energy relates direction to motion at the molecular level. As the temperature rises, molecules move faster and collide more vigorously, greatly increasing the likelihood of bond cleavages and rearrangements as described above.

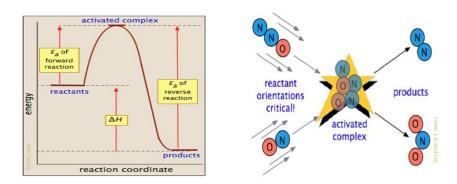


Fig.1 Activation Energy and Activated complex

A general objective of the analysis and prediction of thermally activate reactions is the derivation of a complete description of the progress of a reaction that is valid for any thermal treatment as a

- Isothermal by linear heating
- Non-isothermal treatment

Many researchers make the simplifying assumption that the transformation rate during a reaction is the product of two functions, one depending solely on the temperature T, and the other depending solely on the fraction transformed α

$$\frac{d\alpha}{dt} \\
= f(\alpha)k(t) \tag{1}$$

Temperature dependent function follows Arrhenius type dependency,

$$K_{T} = K_{0} \exp\left(\frac{-E}{R.T}\right)$$
 (2)

The quantity α is the degree of conversion, $f(\alpha)$ is a mathematical function whose form depends on the reaction types and KT is the temperature dependent rate constant K0 is pre exponential factor, E is the activation energy and R is the gas constant, 8.314 J/mol K

From equation (1) and equation (2)

$$\frac{d\alpha}{dt} = K f(\alpha) \exp \left(-\frac{E}{R \cdot T}\right)$$
(3)

II. LITERATURE REVIEW

Borham, B. M. et al [1] studied the urea nitrate by differential thermal analysis (DTA) curves using the Murray and White equation and various other reaction rate equations and An average activation energy ΔE_{\star}^{*} of 31.7 ± 10.0 kcal/mole was calculated and they have shown that These results illustrate the pronounced effect of self-heating on calculation of activation energies. The Kissinger method of calculating the reaction order developed for endothermic DTA peaks produced good results when applied to the present DTA study.

C T Moynihan et al [2]. Studied the activation energy ΔH for structural relaxation in the glass transition region which determined from the heating rate dependence of the glass transition temperature Tg or the cooling rate dependence of the limiting fictive temperature T'f measured using DSC or DTA. The activation energy ΔH for structural relaxation m the glass transition region can be determined from the heating rate dependence of the glass transition temperature Tg or the cooling rate dependence of the limiting fictive temperature T'f measured using DSC or DTA. ΔH values determined this way are in good agreement with the shear viscosity activation energies ΔH n. ΔH n * for high Tg inorganic glasses can also be estimated from the width $\Delta (1/Tg)$ of the glass transition region measured by DSC or DTA using an empirical constant $C = (\Delta H n */R)\Delta (1/Tg)$. New data for sodium borate glasses yield values of the constant C in agreement.

Keuleers, R. R., J. F. Janssens, et al [3] comparison the effective methods for calculation of activation energy for the thermal decomposition of chemical compounds. They have studied for the comparative study of different measurement and calculation procedures for the thermal decomposition of Mn (Urea)2 Cl2.

Starink, M. J, et al [4] studied the Model-free iso-conversion methods which were most reliable methods for the calculation of activation energies of thermally activated reactions and a large number of these iso-conversion methods have been proposed in the literature. Type A methods such as Friedman methods make no mathematical approximations, and Type B methods, such as the generalised Kissinger equation. And they found that accuracy of determination of transformation rates is limited, and type B methods will often be more accurate than type A methods.

Homer E. Kissinger et al [5] studied the Variation of Peak Temperature with Heating Rate in Differential Thermal Analysis and found that Changes in heat content of the active sample are indicated by deflections shown by a line representing the differential temperature. It is conventional to represent an endothermic effect by a negative deflection and an exothermic effect by a positive deflection. The deflections, whether positive or negative, are called peaks.

Masashi Nakamoto et al [6] studied the viscosity of molten slag with low melting point to develop an improved blast furnace operation at lower temperature such as 1673 K. They measured the viscosities of molten CaO- SiO2-MgO-Al₂O₃ slag by rotating cylinder method and compared with the results of the model developed. They showed that slag with composition 35% Al₂O₃-43.1% CaO-7.5% MgO-14.4% SiO₂ has melting temperature below 1673 K and has a viscosity less than 0.6 Pa.s below 1673 K.

Y.S. Lee et al [7] studied the influence of MgO and Al_2O_3 contents on the viscosities of blast furnace slag containing FeO. The viscosities of CaO-SiO2-Al₂O₃-MgO-FeO slag were measured under conditions of C/S 1.35-1.45, 10-18% Alumina, 3.5-10% MgO and 5% FeO. They found that on increasing Al2O3 content, the viscosity of the slag increased at fixed C/S and MgO content. The viscosity of the slag showed a minimum value at around 7% MgO at temperatures above 1723 K. However, it was not significantly changed with varying MgO content.

III. EXPERIMENTAL PROCEDURE

The Experimental Work Is Divided In 'Five' Parts, The Aim Being to determine the Activation Energy of Blast Furnace Slag and Correlate the chemical composition of Slag for proposing the Flow Characteristics that would Give Slag Behavior with Blast Furnace:

- Collected Five Blast Furnace Slag from Steel Plant Contained Different Heat
- To Determine Chemical Composition By Conventional Methods (Chemical Analysis).
- For Estimation of Activation Energy We have done two measurements i.e. DSC & Viscosity measurements
- Flow Characteristics of Sample were carried out on Heating Microscope Analysis
- Microstructure analysis were carried out by Scanning Electron Microscope (SEM)
- Phase Analysis of sample were carried out by X-Ray Diffraction Techniques (XRD)

IV. EXPERIMENTAL DATA

Table. 1 Chemical composition (wt %) of blast furnace slag

| Sr No | SiO ₂ | Al ₂ O ₃ | CaO | MgO | TiO ₂ | Na ₂ O | K ₂ O | Fe ₂ O ₃ | C/S |
|-------|------------------|--------------------------------|-------|-------|------------------|-------------------|------------------|--------------------------------|-------|
| 1 | 31.86 | 16.92 | 38.00 | 10.23 | 0.7 | 0.98 | 0.48 | 0.66 | 1.192 |
| 2 | 33.25 | 16.31 | 38.84 | 10.56 | 0.82 | 1.1 | 0.52 | 0.54 | 1.107 |
| 3 | 32.48 | 17.00 | 35.78 | 11.88 | 0.55 | 1.1 | 0.52 | 0.60 | 1.101 |
| 4 | 31.08 | 17.04 | 36.96 | 11.22 | 0.5 | 1.8 | 0.88 | 0.40 | 1.189 |
| 5 | 34.32 | 16.58 | 36.2 | 9.57 | 0.55 | 1.36 | 0.82 | 0.53 | 1.054 |

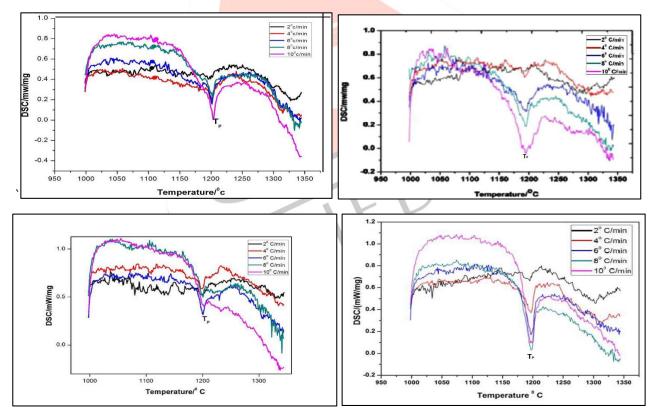


Fig.1 DSC Curves of four powdered slag samples: sample 1, sample 2, sample 3, sample 4, at different heating rates @ 2, 4, 6, 8 and 10^oC/min

Thermal analysis of blast furnace slag is carried out by DSC (Differential Scanning Calorimeter) measurement to determine the crystallization mechanism as mentioned in Section 4.4 and Fig.1 -shows four DSC curves of finely powdered blast furnace slag sample whose C/S ratio 1.192., 1.107, 1.101, and 1.189 respectively.

Calculation based on Activation energy by DSC is based on two different methods which has derived from Arrhenius equation i.e

1. Kissinger Method -

$$\operatorname{Ln}\left(\frac{\emptyset}{\mathsf{T_p}^2}\right) = \frac{-\operatorname{Ea}}{\mathsf{R}.\mathsf{T_p}} + \operatorname{Constan}t \tag{4}$$

2. Ozawa Method -

$$\operatorname{Ln}(\emptyset) = \frac{-\operatorname{E}_{\mathrm{a}}}{\operatorname{T}_{\mathrm{n}}\operatorname{R}} + \operatorname{Constan}t \tag{5}$$

Where

Ø is heating rate in K/min

T_p is peak point temperature in (k) at melting point of slag,

R is universal Gas constant = 8.314 J/mol-k,

Ea is Activation Energy in KJ/mole

Calculation of Peak Temperature from DSC curve of different sample at different heating rate. The glass-transition temperature T_g has determined as the point of intersection of the straight-lines extending from the tangents of the DSC curves in the region of the baseline shift. Some similar features of each thermo gram are apparent

- ullet A reversible endothermic peak at beginning of crystallization temperature, corresponding to the glass-transition temperature $T_{\rm g}$
- Exothermic events with maxima in the range of 1000°C to 1100°C, indicating crystallization temperature T_c
- Endothermic events at about 1280 ${}^{0}\text{C} \pm 1315 {}^{\circ}\text{C}$, involving the melting of some crystal phases, T_{p} (K)

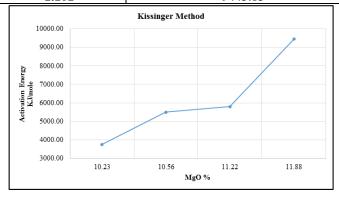
Table 3 Peak temperature of different obtained from DSC Curve

| (°C/min) Heating rate | W ₀ (mg) | T (min.) | T _p (K) Sample: 1 C/S: 1.192 | T _p (K) Sample: 2 C/S: 1.107 | T _p (K) Sample: 3 C/S: 1.101 | T _p (K) Sample: 4 C/S: 1.189 |
|-----------------------------|---------------------|----------|---|---|---|---|
| 2.0 | 25.0 | 287.00 | 1468.8 | 1472.1 | 1466.6 | 1466.6 |
| 4.0 | 25.0 | 199.50 | 1473.2 | 1471.6 | 1466.2 | 1469.2 |
| 6.0 | 25.0 | 170.30 | 1474.2 | 1473.5 | 1467.7 | 1469.5 |
| 8.0 | 25.0 | 155.75 | 1474.8 | 1474.4 | 1467.6 | 1471.3 |
| 10.0 | 25.0 | 147.00 | 1476.8 | 1476.0 | 1468.7 | 1471.2 |

From the given tabulation value and plot between Activation Energy vs. C/s ratio gives the conclusion that As the C/S ratio increases the Activation Energy values decreases and so viscosity of slag decreases due to increase of C/S value basic oxide namely lime, magnesia provide oxygen, act as network breakers and result in depolymerisation of the melt there by decreasing the viscosity

Table. 3 Activation Energy and MgO% by Kissinger and Ozawa Methods

| | Kissinger Method | Ozawa Method | |
|-----------|------------------------------|------------------------------|-------|
| C/S ratio | Activation Energy KJ/mole | Activation Energy KJ/mole | MgO % |
| 1,192 | 3755.10 | 3779.59 | 10.23 |
| 1.107 | 5493.40 | 5518.01 | 10.56 |
| 1.189 | 5790.98 | 5815.35 | 11.22 |
| 1.101 | 9445.83 | 9470.20 | 11.88 |



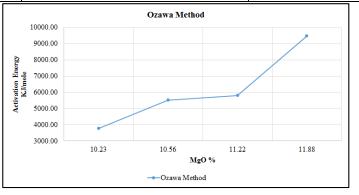


Fig. 2 Graph for Activation energy vs MgO% for Kissinger Method & Ozawa Method

These Graphs shows that as the MgO% increases Activation Energy increases up to 10.56% of MgO contain and then it does not show any significant variation till 11.2% MgO. Beyond 11.22% MgO the Activation Energy again shows an abrupt increase with increase of MgO percentage

In my experimental work calculation of viscosity of blast furnace slag has done by VIS 403 Rotating High Temperature Viscometer which has viscosity range 10¹-10⁸ dPas, Max Temperature 1700⁰C.

In viscosity measurement rate of cooling from liquid phase has adopted 5°C/min. The calculation of viscosity by Arrhenius equation [16] mainly depends on temperature and chemical composition

$$\dot{\eta} = Ae^{\frac{E}{RT}}$$
(6)

Where

ή is viscosity of slag during cooling (d pas),

E is Activation Energy KJ/mole,

R is universal Gas constant =8.314 J/mole,

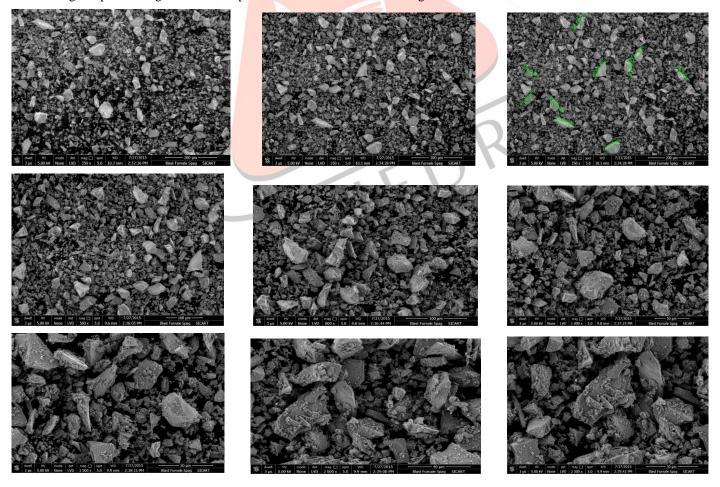
T is Temperature in Kelvin

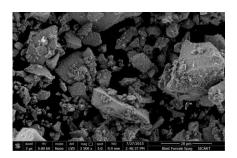
The calculation of viscosity of blast furnace slag has done by the Arrhenius equation. We obtained viscosity 2.95d pas at 1299.3°C of slag sample 4. Which chemical composition is given in Table no 5.6

From this value we have calculated logarithmic value of slag viscosity and this gives the Activation Energy 3906.1002 KJ/mole. Which is approximately same value is as obtained from DSC analysis.

Microstructure

Figure no 3 shows scanning electron microscope images (11 nos of images at different magnification power) of the powder blast furnace slag sample. Average value of sample measure in microstructure images below:





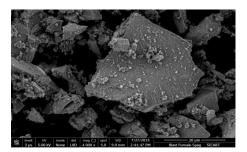


Fig. 3 SEM Microgpahes at at 350 to 4000 magnifications of powder sample having C/S Ratio of 1.192

V. CONCLUSION

- Methods adopted for the calculation of activation energy gave identical values by DSC analysis.
- The values of activation energy obtained by DSC analysis also matched with the results of viscosity measurement
- As the C/S ratio increases the Activation Energy decreases 1.078 and MgO 10.09 to 11.01%) resulting in a short slag.
- As the MgO percentage increases the Activation Energy increases up to 10.56% of MgO and then after 11.22% of MgO abruptly increases Activation Energy
- The calculated value of Activation Energy was much higher may be due to lattice strain in the silicate structure.

VI. REFERENCE

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