

# High presentation of current differencing transconductance amplifier and it's relevance in precision current-mode rectification

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**Abstract** - CMOS based circuit is demonstrated for the realization of the Current Differencing Transconductance Amplifier. The circuit which is projected in this paper can even offer the various benefits with the advantage of broad frequency bandwidth and extremely small input terminal impedance. The simulations and purpose has been illustrated to prove it's remuneration and benefits of the circuit being projected for the means of precise high frequency alteration of the signal.

**IndexTerms** - Current Differencing Transconductance Amplifier, Digital Signal Processing, Current Differencing Buffered Amplifier

## I. INTRODUCTION

It is well known that Current Differencing Transconductance Amplifier ie, CDTA was firstly invented by Biolek in the year 2003 which is liberated from parasitic input capacitances and it could be applied in variety of frequency assortment because of the current mode operation ability of the element. It's block oriented structure is equivalent to CDBA element (Current Differencing Buffered Amplifier) , in which voltage unity gain buffer is used instead of the OTA.

Recently, an increasing number of analog circuits functioning in a current mode has been observed. The mounting interest in current mode analog circuits is caused by the exertion to diminish the supply voltage of the devices up to which it is possible which is especially important in transferable and battery powered apparatus. The bandwidth obtained for current mode circuits is usually higher than for voltage mode circuits created in the same technology. Although the CDTA can be constructed from commercially available integrated circuits, the precise, fast, and temperature-independent applications require utilizing a CDTA chip, implemented in the CMOS or bipolar technology. CDTA may be applied in the CMOS as well as the bipolar technologies. The first published CMOS realization of the CDTA as well as another topology presented in utilized 0.5  $\mu$ m CMOS MIETEC process by means of  $\pm 2.5$ V supply voltages. The work presents the so-called MOCDTA (Multiple Output CDTA) as an extension of the innovative circuit structure from by additional current outputs. The CMOS structure reported in [6] can operate in supply rails down to  $\pm 0.75$  V, utilizing the 0.35  $\mu$ m AMIS technology.

## II. PERFORMANCE OF CDTA

DSP is becoming increasingly more powerful while advances in IC technology provide compact efficient implementation of its algorithms on silicon chips. Although many types of signal processing have indeed moved to digital domain, analog circuits are fundamentally necessary in many of today's complex, high performance systems. This is caused by the reality that naturally occurring signals are analog. Therefore analog circuits act as a bridge between the real world and digital systems. In the beginning, operational amplifiers were the main building blocks for analog circuit design. Unfortunately, their limited performance such as bandwidth, slew-rate etc. led the analog designer to search for other possibilities and other building blocks. Proper symbol of the element called CDTA can be seen in fig.1 with the corresponding circuit of CDTA is described in fig.2

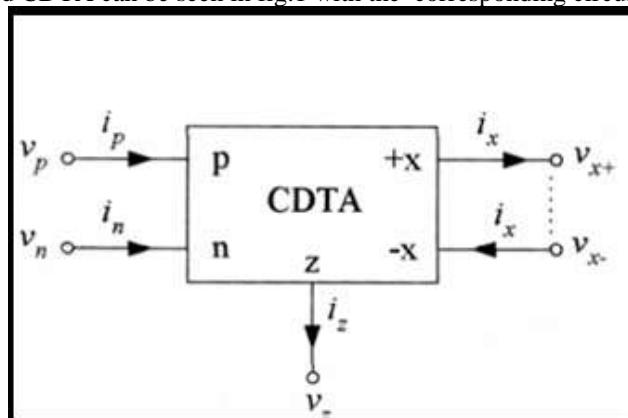


Fig.1. Symbol of CDTA[19]

The connection between the terminals of CDTA could be characterized and are explained as follows:

$$v_p = v_n = 0$$

$$i_z = i_p - i_n$$

$$i_{x+} = g_m v_z = g_m Z_z i_z, i_{x-} = -g_m v_z = -g_m Z_z i_z \tag{1}$$

By going through the above relations between the characteristic equations it can be said that p,n will be the terminals of input and  $Z_z$  would be the external impedance associated at the next port named as 'Z'. The difference of the current will be followed by the current source for the particular application which would be done between the two terminals p and n respectively which makes it's way from Z port to the impedance  $Z_z$ . The terminal z suffers from the voltage drop and thus drop of voltage is given away to the x port which will have certain current in it which is denoted by  $i_x$  from the transconductance gain denoted by  $g_m$ . This will be opportunate by electronic means subsequently to the outside bias current. CDTA is a self possessed device of unity gain source of current and there are two inputs to the current and amny outputs to the transconductance amplifier so that the modifications could be made by the means of electronics by the itinerary of the gain of transconductance offered by the device for the particular application. This has made our experiments very easy and the device proper appropriate in favor of the production of current-mode filters in the midst of electronically tenability characteristics. Additionally, this device could be used in many applications so that the whole experimental results could be found out for the production of filters made on the basis of their current mode operation.

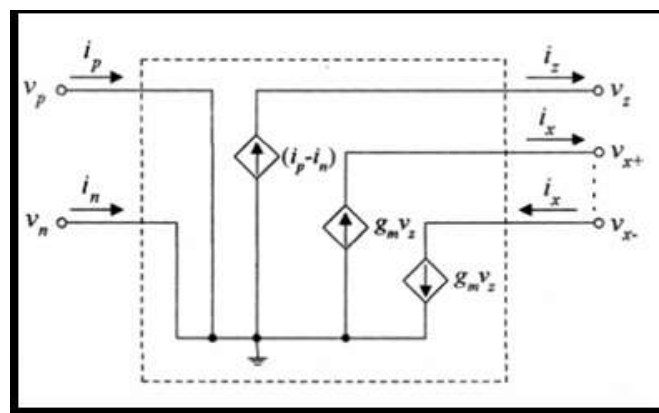


Fig.2 Equivalent model of CDTA[21]

With a rigorous quantity of acquiescent fundamentals the required block can therefore make it able to perform in that particular environment. By this way the thick and strong blocks could be achieved in variety of experiments in the practical manner. The element CDTA becomes forthcoming in many ways so as to realize the continuous processing of the signal of time repeatedly in all the equipments one after other without any disturbances.

• **Behaviour of CDTA**

Every electronics element shows ideal and practical behaviour. current differencing transconductance amplifier also shows ideal and practical behaviour. From matrix equation (1.4) and (1.5) we can get the ideal and practical behaviour of CDTA. The principle performance may be elaborated as follows:

$$I_z = I_p - I_n, I_x = \pm g_m V_z \tag{2}$$

Practical behaviour associated with CDTA is described as follows:

$$I_z = \alpha_p I_p - \alpha_n I_n \text{ and } I_x = +g_m V_z \tag{3}$$

current gains are defined by  $\alpha_p$  and  $\alpha_n$ ,  $\alpha_p = 1 - \epsilon_p$ , and  $\alpha_n = 1 - \epsilon_n$ . their complete ideals which are greatly less than the unity.

**III. MOS-BASED CDTA IMPLEMENTATION**

We know how to correspond to the transistor level demonstration of the projected CDTA as shown in figure 1.3. The number of transistors used in the desired circuit will be twenty seven. If we wish to find out the difference of current then the transistors named from one to seventeen would be taken into account. In greed of low impedance from the circuit the project must be offered by the voltage buffers moreover prolongs with the ports for the input values which are in very small extent by means of implicit ground. The difference of signals at input sides are exceeded by the current mirrors. By this way the outward appearance of DO OTA could be figured out eventually all this is done by the self assured inverting kinds of amplifiers .

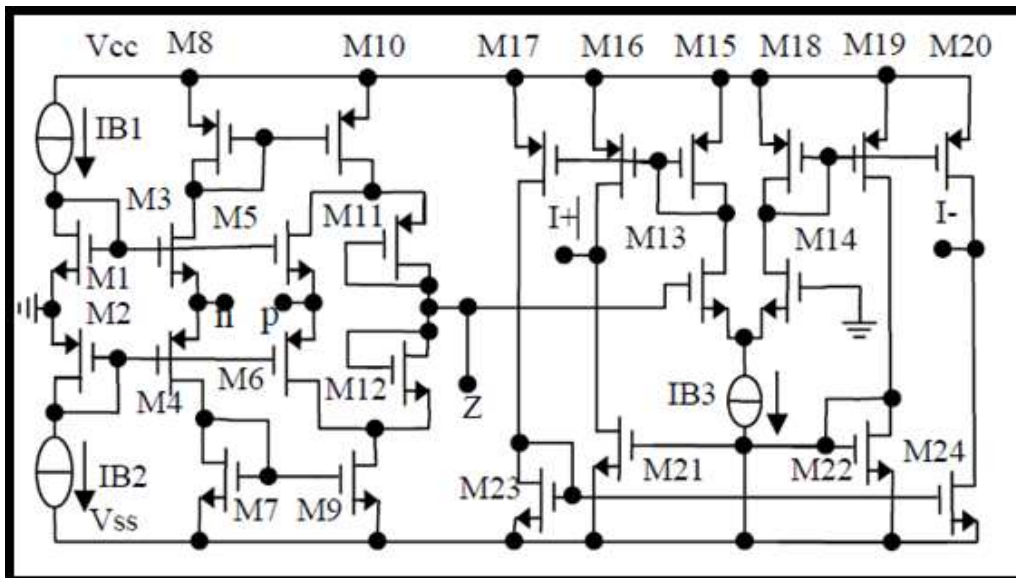


Fig.3 CMOS-based CDTA implementation[1]

IV. PRECISION RECTIFIER USING CDTA

This defines high performance CDTA and its function within precision current mode rectification. The figure 3. properly describes the current mode full wave rectifier which is utilized only by the means of a CDTA. The documented customary of the alteration of element may be visualized with the help of representation of the required circuitry. Now the main thing is to place single CDTA instead of two positive current conveyors. The gain of current is positioned by the external resistance R and the value of R will be taken as  $1/g_m$ . In order to get a unit gain current the gain could be furthermore be proficiencies by just making it free from the resistor and the auxiliary current can be injected into the terminal. If the DC value is appropriately handled and applied the current tracking errors and the offsets of current that causes some DC imperfections. The enduring element of the rectifier that is diodes and the  $R_{load}$ . Also bias circuitry is examined thoroughly and specified properly. When it is to be closed between the off and on conditions of current  $I_{aux}$  that causes some DC imperfections. The enduring element of the rectifier that is diodes and the  $R_{load}$ . Also bias circuitry is examined thoroughly and specified properly. To get rid of the postponement awakened by diodes at the same time as switching between the ON and OFF conditions and numerous kinds of DC biasing can take place into the account of the desired representation and its behavior.

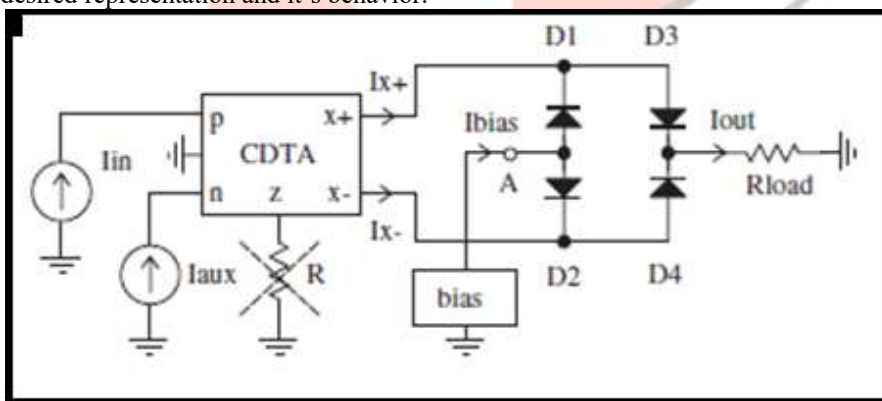
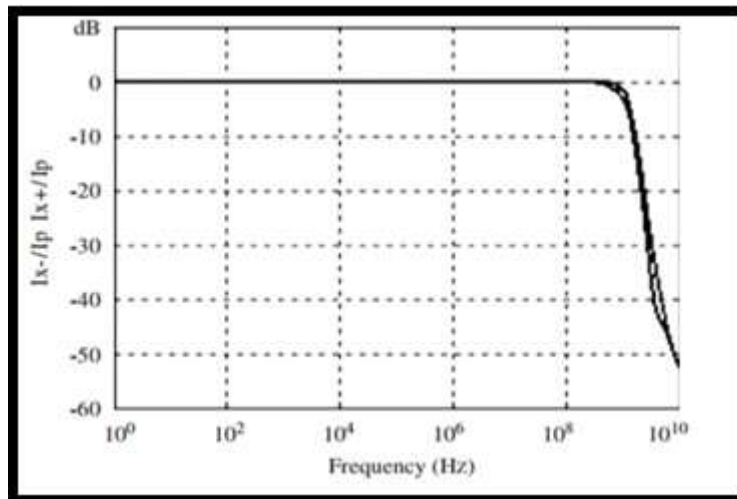


Fig.4 Full-wave rectifier based on current mode circuit where resistor R could be absent[1]

V. RESULT

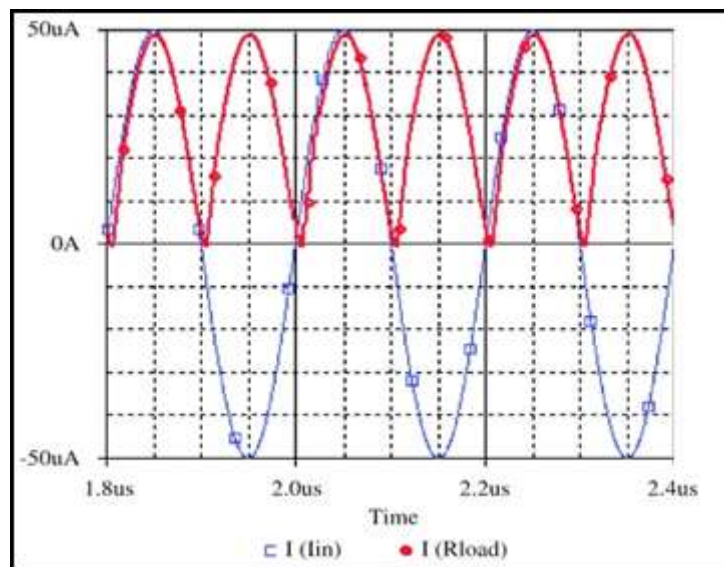
A high performance CDTA with its application in precision current mode rectification is defined and explained in this section. Simulations of the projected CMOS CDTA and precision rectifier could be prepared by means of PSPICE with TSMC 0.35µm n-well CMOS procedure. Power supplies are chosen as  $V_{dd} = -V_{ss} = 1.8V$ . The dimension of the  $M_{12}$  is not equal to that of the  $M_{11}$  to terminate the increasing error.  $M_{21}$  has not the equivalent size with  $M_{23}$ ; and  $M_{26}$  has not the similar size with  $M_{25}$ ,  $M_{27}$ , and  $M_{28}$  to abandon offset and level-shift errors. Bias current  $I_B$  is elected as  $40\mu A$ . The projected CDTA shows the mechanism near the GHz range. Figure. 3.8 shows the -3 dB bandwidths of the current gains  $I_{x+}/(I_p - I_n)$  and  $I_{x-}/(I_p - I_n)$ , that are positioned at 1011MHz and 1230MHz correspondingly, for  $R_z = 1160\Omega$  and  $I_n = 0A$ . The transconductances  $g_m$  of DO-OTA for  $V_z = 1V$  DC are 873 and  $882\mu A/V$  for  $I_{x+}/V_z$  and  $I_{x-}/V_z$ , correspondingly, and  $882\mu A/V$  for  $I_{x+}/V_z$  and  $I_{x-}/V_z$ , correspondingly.

If we wish to visualize the simulated results by using SPICE for full wave rectifier then it could be done by means of diodes known as schottky diodes 1PS79SB63. Figure 5. exhibits the acceptable process while rectifying the  $50\mu A/5MHz$  that would be a sine wave. If the output of the waveforms are considered and we wish to improve those characteristics then definitely the diode characteristics. This will define the performance and to improve or to degrade both is in the hands of the self motivated diode which would not be present in the CDTA. The exceptional presentation can be seen having 5MHz of frequency..



**Fig. 5– AC simulation outcomes of CDTA designed for  $I_{x+} / (I_p - I_n)$  and  $I_{x-} / (I_p - I_n)$  for  $R_z = 1160\Omega$**

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**Fig.3.8 Rectified sine waveform of 5MHZ  $R_{load} = 1\Omega$ ,  $R = 1.21k\Omega$ ,  $I_{bias} = 1.2 \mu A$ ,  $I_{aux} = 0.7 \mu A$ .**

## VI. CONCLUSION

In this study, a novel precision rectifier circuit using a high-performance CMOS-based CDTA structure is presented. The high-performance CMOS-based CDTA organization takes advantage for the huge bandwidth and close-to-ideal terminal impedances. The proposed circuit is suitable for monolithic integrated circuit implementation. CDTA-based precision full-wave rectifier described in this study is highly successful in high frequency procedure just because of the environment shown by current-mode operation.

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