

Comparative Linear Time History Analysis of Reinforced Concrete Buildings With Changing Frequency Content Using Staad Pro

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Abstract - Proper selection of seismic design forces for engineering structures requires specification of the expected intensity of ground shaking that the structure will experience during their lifetime. In order to take precaution for the loss of lives and damage of structures subjected to ground motion, it's important to understand the characteristics of ground motion. The most important dynamic characteristics of ground motion are peak ground acceleration (PGA), frequency content and duration. The more common practice adopted by many seismic codes is to use peak acceleration as a single measure of ground motion intensity. However, as more earthquake records were obtained, it became apparent that the use of a single design spectral shape scaled by peak site acceleration is inadequate to cover over all sites. Many recorded earthquake ground motions have response spectra dramatically different from the standard design spectrum. Ground motions have varying frequency contents as low, intermediate and high. Present work studies the effect of varying frequency content of ground motion on reinforced concrete buildings. Linear time history analysis is performed in STAAD Pro software on regular 3D two, six and twenty storey R.C. buildings with six ground motions of low, intermediate and high frequency contents having same duration and peak ground acceleration. The response of buildings due to the ground motions in terms of story displacement, story velocity, story acceleration and base shear are found. The results show that low-frequency content and intermediate-frequency content ground motions have significant effect on regular R.C. buildings. However, high-frequency content ground motions have very less effect on responses of the regular R.C. buildings.

Keywords - Ground Motion, Peak Ground Acceleration, Frequency Content, Linear Time History Analysis, Base shear, Storey displacement

I. INTRODUCTION

The earth vibrates continuously at periods ranging from milliseconds to days and the amplitudes may vary from nanometers to meters. The motion that affects living beings and their environment is of interest for engineers and is termed as Strong ground motion. The Motion of the ground can be described in terms of displacement, velocity and acceleration. The variation of ground acceleration with time, recorded at a point on the ground during an earthquake is called an accelerogram. The ground velocity and displacement can be obtained by direct integration of an accelerogram. Typical ground motion records are called time histories. From an engineering point of view, the peak ground acceleration, frequency content and the duration of motion are the three important characteristics of the ground motion parameters. These characteristics play predominant role in studying the behavior of structures under the seismic ground motions.

The responses of R.C. buildings are strongly dependent on the frequency content of the ground motions. The frequency content (distribution of energy with respect to frequencies) of an accelerogram is represented by Fourier spectrum, Power spectrum and Response spectrum. Inspection of earthquake records (Zhu 1985) has revealed that ground motions with a high frequency content in the strong-motion phase generally correspond to high a/v ratios, whereas those containing intense, long-duration acceleration pulses generally are associated with low a/v ratios. Ground motions at moderate distances from the energy source normally have a broad range of significant frequency content, resulting in intermediate a/v ratios. Therefore, the a/v ratio provides information on the frequency characteristics of ground motions in a statistical sense.

Based on the frequency content (PGA/PGV) ground motion records have been classified into following categories-

| | |
|--------------------------------|-----------------------------|
| High frequency content | $PGA/PGV > 1.2$ |
| Intermediate frequency content | $0.8 \leq PGA/PGV \leq 1.2$ |
| Low frequency content | $PGA/PGV < 0.8$ |

The ratio of peak ground acceleration in terms of acceleration (g) to peak ground velocity (m/s) is defined as the frequency content of ground motion. The present work shows low, mid and high rise reinforced concrete buildings responses under low, intermediate and high frequency content ground motions.

II. OBJECTIVES

The objectives of the study were-

- 1) To study the seismic behavior of regular R.C.C. buildings resting on leveled ground under varying frequency content ground motions.
- 2) To carry out time history analysis for different cases by varying the height of the R.C.C. buildings resting on leveled ground.
- 3) To compare the seismic behavior of R.C.C. buildings under varying frequency content ground motions in terms of Storey displacement and base shear.

III. METHODOLOGY

The methodology, which was conducted, is briefly described as below:

- 1) To collect Ground motion records and then to normalize them.
- 2) To perform Time history analysis using relevant Finite Element Method based software.
- 3) Building response such as storey displacement, storey velocity, storey acceleration and base shear are found corresponding to ground motions.
- 4) The result of R.C.C. buildings resting on leveled ground are compared with respect to the varying frequency content ground motions.

Ground Motion Data

The following six ground motion records having low, intermediate and high frequency content are considered for analysis:

- [1] 1979 Imperial Valley-06 (Holtville Post Office) H-HVP225 component
- [2] IS 1893 (Part1) : 2002 (Artificial ground motion)
- [3] 1957 San Francisco (Golden Gate Park) GGP010 component
- [4] 1940 Imperial Valley (El Centro) elcentro_EW component
- [5] 1992 Landers (Fort Irwin) FTI000 component
- [6] 1983 Coalinga-06 (CDMG46617) E-CHP000 component

Ground motion characteristics and classification of its frequency-content

| Record | Component | Magnitude | Epicentral Distance (km) | Duration (s) | Time step for response computation (s) | PGA (g) | PGV (m/s) | PGA/PGV | Frequency Content Classification |
|---|-------------|-----------|--------------------------|--------------|--|---------|-----------|---------|----------------------------------|
| 1979 Imperial Valley-06 (Holtville Post Office) | H-HVP225 | 6.53 | 19.81 | 37.74 | 0.005 | 0.2526 | 0.4875 | 0.5182 | Low |
| IS 1893 (Part1) : 2002* | - | - | - | 38.01 | 0.01 | 1 | 1.0407 | 0.9609 | Intermediate |
| 1957 San Francisco (Golden Gate Park) | GGP010 | 5.28 | 11.13 | 39.72 | 0.005 | 0.0953 | 0.0391 | 2.4405 | High |
| 1940 Imperial Valley (El Centro) | elcentro_EW | 7.1 | - | 53.46 | 0.02 | 0.2141 | 0.4879 | 0.4389 | Low |
| 1992 Landers (Fort Irwin) | FTI000 | 7.28 | 120.99 | 39.98 | 0.02 | 0.1136 | 0.0957 | 1.1868 | Intermediate |
| 1983 Coalinga-06 (CDMG46617) | E-CHP000 | 4.89 | 9.27 | 39.995 | 0.005 | 0.1479 | 0.0573 | 2.5810 | High |

Ground motion characteristics and classification of its frequency-content for 40 s duration

| Records | Component | Magnitude | Epicentral Distance (km) | Duration (s) | Time step for response computation (s) | PGA (g) | PGV (m/s) | PGA/PGV | Frequency Content Classification |
|---|-----------|-----------|--------------------------|--------------|--|---------|-----------|---------|----------------------------------|
| 1979 Imperial Valley-06 (Holtville Post Office) | H-HVP225 | 6.53 | 19.81 | 40 | 0.005 | 0.2526 | 0.4875 | 0.5182 | Low |

| | | | | | | | | | |
|---------------------------------------|--------------|------|--------|----|-------|--------|--------|--------|--------------|
| Office) | | | | | | | | | |
| IS 1893 (Part1) : 2002 | - | - | - | 40 | 0.01 | 1 | 1.0407 | 0.9609 | Intermediate |
| 1957 San Francisco (Golden Gate Park) | GGP010 | 5.28 | 11.13 | 40 | 0.005 | 0.0953 | 0.0391 | 2.4405 | High |
| 1940 Imperial Valley (El Centro) | elcentr0_E W | 7.1 | - | 40 | 0.02 | 0.2141 | 0.4879 | 0.4389 | Low |
| 1992 Landers (Fort Irwin) | FTI000 | 7.28 | 120.99 | 40 | 0.02 | 0.1136 | 0.0957 | 1.1868 | Intermediate |
| 1983 Coalinga-06 (CDMG46617) | E-CHP000 | 4.89 | 9.27 | 40 | 0.005 | 0.1479 | 0.0573 | 2.5810 | High |

IV. MODELING OF STRUCTURE AND PROBLEM DISCUSSION

In order to evaluate the seismic response of buildings with rigid floor diaphragms using dynamic (Linear Time History) analysis procedures two sample buildings were adopted the details of these buildings are produced in section. The seismic analysis software STAAD Pro is utilized to create model and run all analyses. The software is able to predict the geometric nonlinear behavior of space frames under static or dynamic loadings, taking into account both geometric nonlinearity and material inelasticity. The software accepts static loads (either forces or displacements) as well as dynamic (accelerations) actions and has the ability to perform eigenvalues, and linear dynamic analyses.

Details Of the Model 1

For this study, a 2-story building with 2x5 bays and floor height 3.5 m, regular in plan was considered. This building is considered to be situated in seismic zone III and designed in compliance to the Indian Code of Practice for Earthquake Resistant Design of Structures. The building is considered to be fixed at the base. The building is modeled using software STAAD Pro.

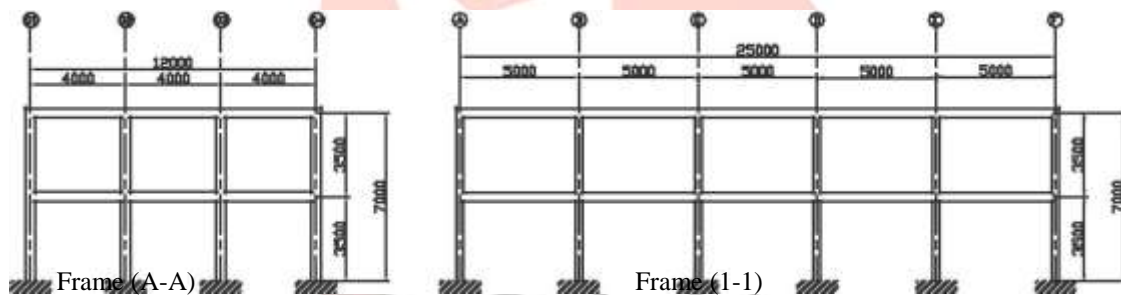
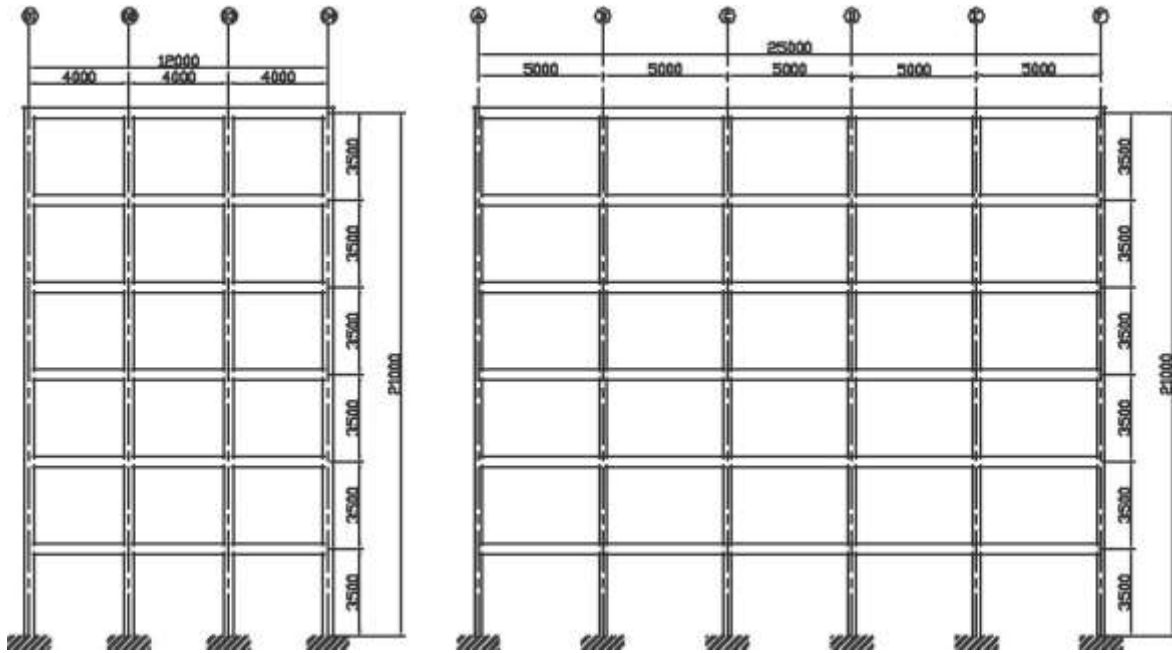


Figure 1: Frame (A-A) and (1-1) of two-story regular R.C. building (all dimension in mm)

Details Of the Model 2

For this study, a 6-story building with 3x5 bays and floor height 3.5 m, regular in plan is considered. This building is considered to be situated in seismic zone III and designed in compliance to the Indian Code of Practice for Earthquake Resistant Design of Structures. The building is considered to be fixed at the base. The building is modeled using software STAAD Pro.



Frame (B-B)

Frame (2-2)

Figure 2: Frame (B-B) and (2-2) of six-story regular R.C. building (all dimension in mm)**Details Of the Model 3**

For this study, a 20-story building with 3x5 bays and floor height 3.5 m, regular in plan is considered. This building is considered to be situated in seismic zone III and designed in compliance to the Indian Code of Practice for Earthquake Resistant Design of Structures. The building is considered to be fixed at the base. The building is modeled using software STAAD Pro.

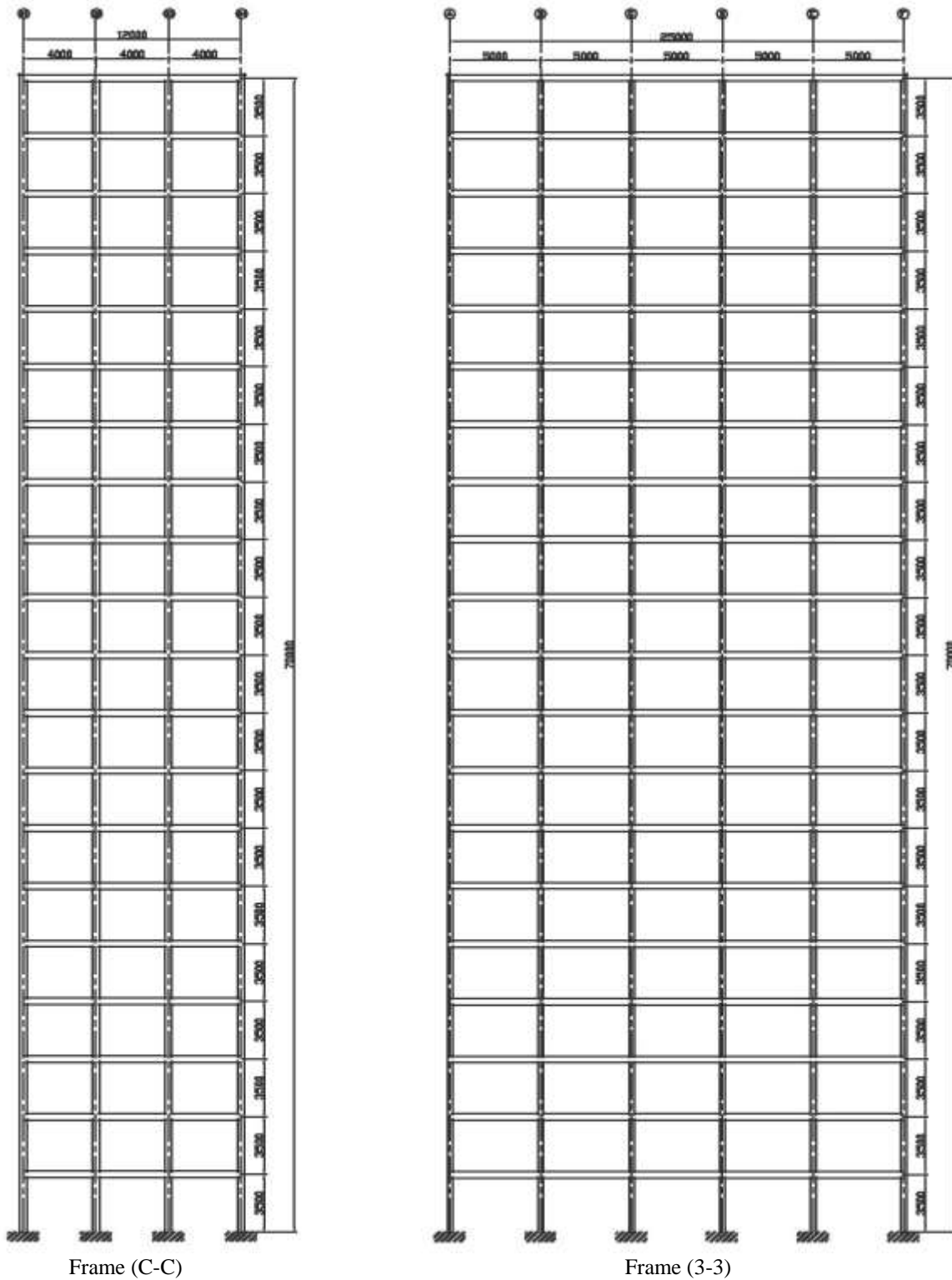


Figure 3: Frame (C-C) and (3-3) of twenty-story regular R.C. building (all dimension in mm)

Table 1: Gravity loads assigned to the R.C. buildings

| Gravity Load | Value |
|-------------------------|---------------------------|
| Slab load (dead load) - | 3.0 (KN/m ²) |
| Wall load (dead load) - | 17.50 (KN/m) |
| Live load - | 3.50 (KN/m ²) |

Table 2: Concrete and steel bar properties as per IS 456

| Concrete Properties | Steel Bar Properties |
|---------------------|----------------------|
|---------------------|----------------------|

| | | | |
|-----------------------|-------------------------|-----------------------|-----------------------------|
| Unit weight | 25 (KN/m ³) | Unit weight | 76.973 (KN/m ³) |
| Modulus of elasticity | 22360.7 (MPa) | Modulus of elasticity | 2 x 10 ⁵ (MPa) |
| Poisson ratio | 0.2 | Poisson ratio | 0.3 |
| Thermal coefficient | 5.6 x 10 ⁻⁶ | Thermal coefficient | 1.17 x 10 ⁻⁶ |
| Shear modulus | 9316.95 (MPa) | Shear modulus | 76923.10 (MPa) |
| Damping ratio | 5 (%) | Yield strength | 415 (MPa) |
| Compressive strength | 30 (MPa) | Tensile strength | 485 (MPa) |

Table 3: Beam and column length and cross section dimension

| Structural Element | Cross section (mm x mm) | Length (m) |
|-----------------------|-------------------------|------------|
| Beam in (x) direction | 300 x 400 | 4.0 |
| Beam in (z) direction | 300 x 400 | 5.0 |
| Column | 300 x 400 | 3.45 |

V. RESULTS AND DISCUSSION

Results for Model 1

For the model 1 Linear dynamic Analysis (Linear Modal Time History Analysis) is carried out with varying frequency content ground motions.

| Storey | First | | | | | | Second | | | | | | |
|----------------------------------|-------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|--|
| | 1 | 2 | 3 | 4 | 5 | 6 | 1 | 2 | 3 | 4 | 5 | 6 | |
| Ground Motion | | | | | | | | | | | | | |
| Displacement (mm) | 13.8 | 15.73 | 4.98 | 17.15 | 12.56 | 8.04 | 22.63 | 26.24 | 8.43 | 28.32 | 21.05 | 12.89 | |
| Velocity (mm/s) | 221.6 | 254.1 | 101.2 | 223.8 | 200.6 | 152.4 | 354.5 | 427.8 | 162.4 | 358.8 | 325.7 | 251.1 | |
| Acceleration (m/s ²) | 3.726 | 4.532 | 2.548 | 3.650 | 3.201 | 2.568 | 6.204 | 7.358 | 4.015 | 5.981 | 5.016 | 4.023 | |

Storey displacement, velocity and acceleration of two-storey regular reinforced concrete building due to ground motion GM1 to GM6 in x direction

| Storey | First | | | | | | Second | | | | | | |
|----------------------------------|-------|-------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|--|
| | 1 | 2 | 3 | 4 | 5 | 6 | 1 | 2 | 3 | 4 | 5 | 6 | |
| Ground Motion | | | | | | | | | | | | | |
| Displacement (mm) | 24.14 | 18.73 | 6.18 | 31.15 | 24.35 | 10.04 | 37.45 | 31.24 | 8.23 | 47.32 | 37.27 | 14.89 | |
| Velocity (mm/s) | 252.6 | 254.1 | 89.2 | 389.8 | 300.6 | 122.4 | 374.5 | 387.8 | 134.4 | 582.8 | 455.7 | 183.1 | |
| Acceleration (m/s ²) | 3.236 | 4.232 | 2.348 | 3.950 | 3.111 | 2.258 | 6.644 | 7.898 | 4.255 | 5.751 | 5.246 | 4.353 | |

Storey displacement, velocity and acceleration of two-storey regular reinforced concrete building due to ground motion GM1 to GM6 in z direction

GM1- 1979 Imperial Valley-06 (Holtville Post Office) HVP225 component (low frequency content)

GM2- IS 1893 (Part1) : 2002 (intermediate frequency content)

GM3- 1957 San Francisco (Golden Gate Park) GGP010 component (high frequency content)

GM4- 1940 Imperial Valley (El Centro) elcentro_EW component (low frequency content)

GM5- 1992 Landers (Fort Irwin) FTI000 component (intermediate frequency content)

GM6- 1983 Coalinga-06 (CDMG46617) E-CHP000 component (high frequency content)

Base shear of two-storey regular R.C. building subjected to ground motion GM1 to GM6 in x and z direction

| Direction | Base Shear (KN) | | | | | |
|-----------|-----------------|---------|--------|---------|---------|---------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| X | 2750.11 | 3111.41 | 981.81 | 3350.56 | 2444.39 | 1591.42 |
| Z | 3001.41 | 2453.82 | 652.36 | 3828.29 | 3018.53 | 1235.86 |

Results for Model 2

For the model 2 Linear dynamic Analysis (Linear Modal Time History Analysis) is carried out with varying frequency content ground motions.

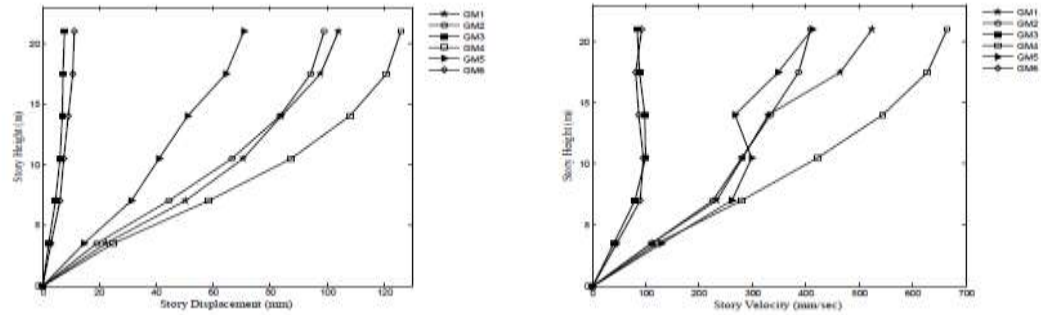


Figure 5.10: Story displacement, velocity, and acceleration of six-story regular reinforced concrete buildings due to ground motion GM1, GM2, GM3, GM4, GM5, and GM6 in x-direction

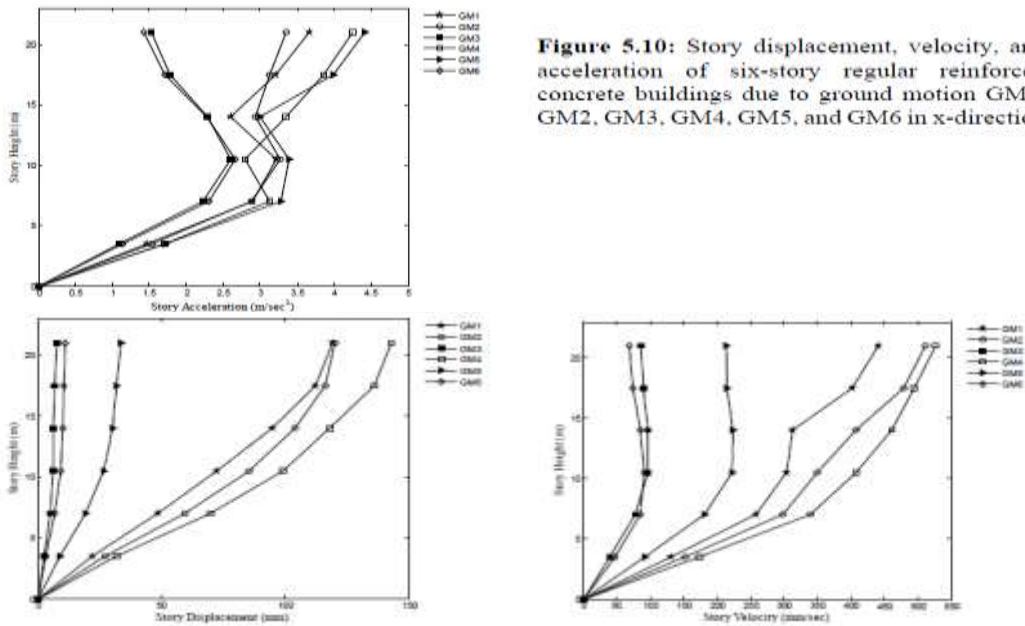


Figure 5.11: Story displacement, velocity, and acceleration of six-story regular reinforced concrete buildings due to ground motion GM1, GM2, GM3, GM4, GM5, and GM6 in z-direction

Base shear of six-storey regular R.C. building subjected to ground motion GM1 to GM6 in x and z direction

| Direction | Base Shear (KN) | | | | | |
|-----------|-----------------|---------|---------|---------|---------|---------|
| | X | 3822.94 | 3199.36 | 376.88 | 4164.58 | 2584.60 |
| Z | 2504.07 | 3043.55 | 284.34 | 3587.44 | 1065.70 | 392.42 |

Results for Model 3

For the model 3 Linear dynamic Analysis (Linear Modal Time History Analysis) is carried out with varying frequency content ground motions.

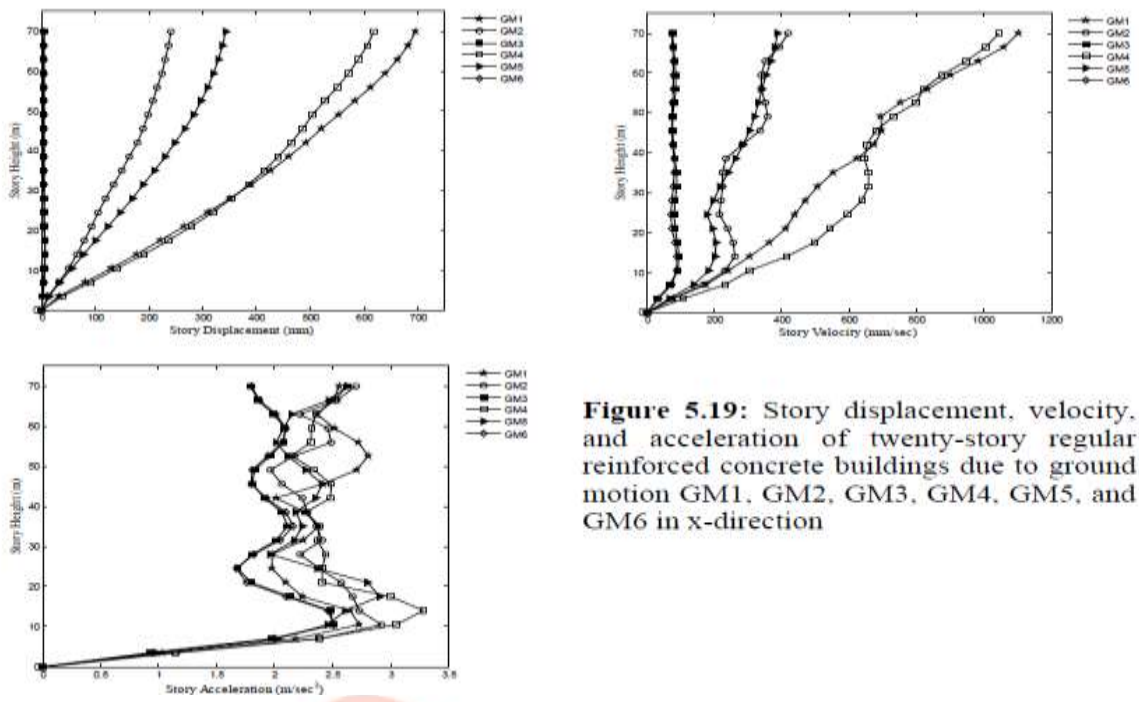


Figure 5.19: Story displacement, velocity, and acceleration of twenty-story regular reinforced concrete buildings due to ground motion GM1, GM2, GM3, GM4, GM5, and GM6 in x-direction

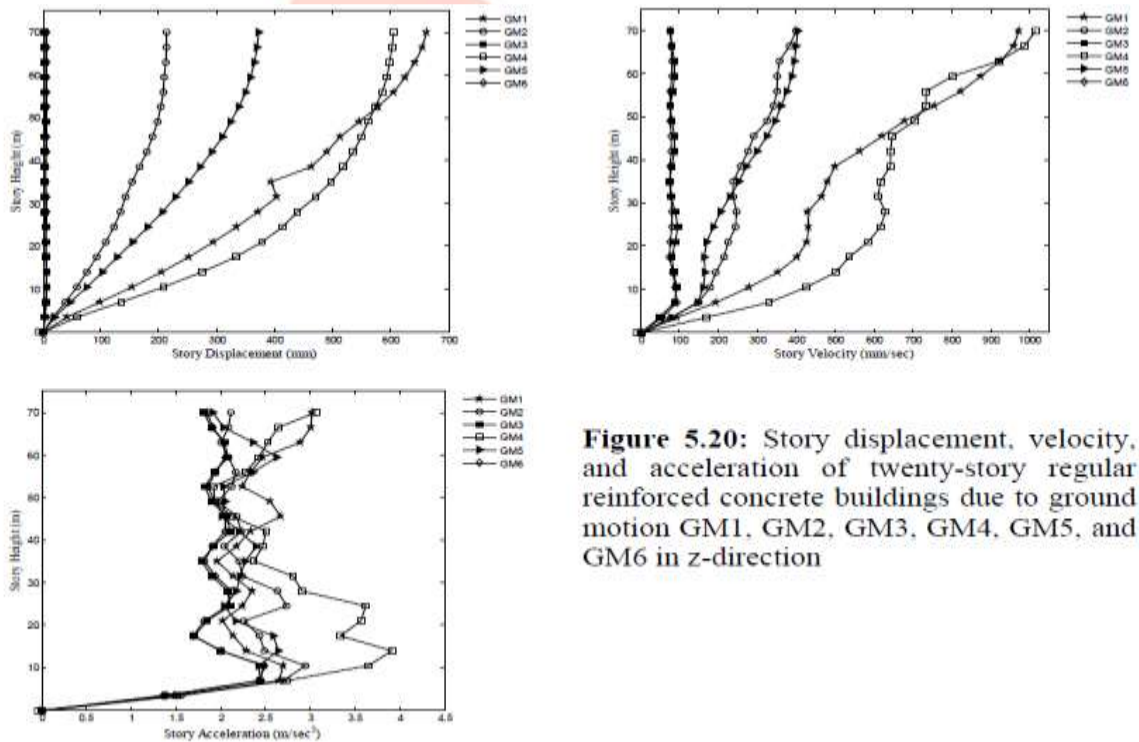


Figure 5.20: Story displacement, velocity, and acceleration of twenty-story regular reinforced concrete buildings due to ground motion GM1, GM2, GM3, GM4, GM5, and GM6 in z-direction

Base shear of twenty-story regular R.C. building subjected to ground motion GM1 to GM6 in x and z direction

| Direction | Base Shear (KN) | | | | | |
|-----------|-----------------|---------|---------|---------|---------|---------|
| | X | 5367.09 | 2242.74 | 355.83 | 6437.29 | 2215.18 |
| Z | 4608.20 | 1934.90 | 338.98 | 6538.69 | 2229.92 | 378.76 |

Effects Of earthquake frequency contents

A 2-story, 6-story and 20-story R.C. building regular in plan were subjected to six varying earthquake frequency content ground motions was considered and analyzed using STAAD Pro. Response quantities like story displacement (R00f), base shear were extracted. 2-story, 6-story and 20-story regular RC building experienced maximum story displacement (R00f) due to low frequency content ground motions in X and Z direction and minimum story displacement (R00f) due to high frequency content ground motions in X and Z direction and medium story displacement (R00f) due to intermediate frequency content ground motions in X and Z direction. They experienced maximum base shear due to low frequency content ground

motions in X and Z direction and minimum base shear subjected to high frequency content ground motions in X and Z direction and medium base shear subjected to intermediate frequency content ground motions in X and Z direction.

VI. CONCLUSION

The maximum and minimum values of storey displacement, storey velocity, storey acceleration and base shear of two, six and twenty storey regular R.C. building subjected to GM1 to GM6 in x and z direction are shown in Table given below-

| R.C. Building | Two-Storey | | | | Six-Storey | | | | Twenty-Storey | | | |
|----------------------|------------|------|------|------|------------|------|------|------|---------------|------|------|------|
| | (x) | | (z) | | (x) | | (z) | | (x) | | (z) | |
| Ground motion | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. | Max. | Min. |
| Storey displacements | 4 | 3 | 4 | 3 | 4 | 3 | 4 | 3 | 1 | 3, 6 | 1 | 3, 6 |
| Storey Velocity | 2 | 3 | 4 | 3 | 4 | 3, 6 | 4 | 6 | 1 | 3, 6 | 4 | 3, 6 |
| Storey Acceleration | 2 | 3, 6 | 4 | 3 | 5 | 6 | 4 | 6 | 4 | 3, 6 | 4 | 3, 6 |
| Base Shear | 4 | 3 | 4 | 3 | 4 | 3 | 4 | 3 | 4 | 3 | 4 | 3 |

1, 2, 3, 4, 5, and 6 represents the ground motion serial number

REFERENCES

- [1] "Structural Analysis And Design (STAAD Pro) software," Bentley Systems, Inc.
- [2] A.Baghchi, Evaluation Of the Seismic Performance Of Reinforced Concrete Buildings, Ottawa: Department Of Civil and Environmental Engineering, Carleton University, 2001.
- [3] T. Cakir, "Evaluation Of the effect Of earthquake frequency content On seismic behavior Of cantiliver retaining wall including soil-structure interaction," Soil Dynamics and Earthquake Engineering, vol. 45, pp. 96-111, 2013.
- [4] S. K. Nayak and K. C. Biswal, "Quantification Of Seismic Response Of Partially Filled Rectangular Liquid Tank with Submerged Block," Journal Of Earthquake Engineering, 2013.
- [5] "Pacific Earthquake Engineering Research Center: NGA Database," 2005. [Online]. Available: <http://peer.berkeley.edu/nga/data?doi=NGA0185>. [Accessed 2013].
- [6] IS 1893 (Part1), Indian Standard CRITERIA FOR EARTHQUAKE RESISTANT DESIGN OF STRUCTURES PART 1, 6.1 ed., New Delhi 110002: Bureau Of Indian Standards, 2002.
- [7] "Pacific Earthquake Engineering Research Center: NGA Database," 2005. [Online]. Available: <http://peer.berkeley.edu/nga/data?doi=NGA0023>. [Accessed 2013].
- [8] "Vibration Data El Centro Earthquake," [Online]. Available: <http://www.vibrationdata.com/elcentro.htm>. [Accessed 2013].